Final Design Report ECE 362 5/24/2022 Team 08: Burnt Hotdog Tyra Correia, Andrew Shaw, Neha Vinesh, and Noah Young

### **Executive Summary:**

The purpose of this design project is to demonstrate engineering techniques like programming and circuit design on a car that will inspire high school students to pursue an education in STEM. In our car, we will use a microcontroller to handle the control signals and computations required to steer the car along a line, and this microcontroller will be able to communicate information about the current state of the car to the user during operation. To provide power to the vehicle, we will use an energy storage system capable of quickly recharging, internally balancing the energy stored within each of its constituent stages, and providing a consistent output of power to the motor controller on the vehicle. All features to be implemented to achieve these design goals will be created with both safety and creativity in mind, and special importance will be put on the overall system's usability and reliability so that the vehicle can promote learning for people with various backgrounds of engineering.

#### **Stakeholders/Features/Metrics:**











# **Interactions Model:**



## **Functional Architecture Model:**



# **Physical Design Solution Models:**



## Software Flow Diagram:

Figure 1: Software Flowchart Diagram. This code establishes/begins various modules (bluetooth, INA219, servo, and huskylens) to collect and interpret data to then execute various decisions to both track and follow the line on the track.

Energy input system:



Figure 2: Initial energy input circuit design schematic (Note that the boost converter and all supporting components shown in the center of this image were replaced by the boost converter module shown in Fig. 3 in the final design implementation)

The energy input circuit schematic found in Figure 2 can be mapped to the control charging block of the functional architecture model and is composed of a power source selection circuit, a boost converter, and a current limiting circuit. The energy input circuit schematic is designed such that the power selection circuit automatically toggles between wired and wireless charging depending on if the wired charger is plugged into the power supply.

#### Subsystems:

- Wired charger (not pictured): The wired charger will use a 120V AC to 12V DC wall power supply capable of supplying up to 5A.
- Wireless charger (not pictured):

The wireless charger will use a USB-C power input and will be capable of providing 12V DC at the receiver coil at currents up to 2A.

Power source selector:



Figure 3: Power source selection circuit schematic

To switch between the wired and wireless power, the PR12-24V-360 relay is used to toggle between the respective sources when its coil is energized by the connection of the 12 wired charger. The schematic for the power source selection circuit can be found in Figure 3. This effectively satisfies requirements FP2.3, FP2.4 and FP3.0.

#### - Boost converter:

Gowoops 5PCS 150W DC-DC 10-32V to 12-35V Step Up Boost Converter Module Adjustable Power Voltage



Figure 4: Boost converter module (Note that because this module came in a pack of 5, the cost added to the bill of materials only reflects one fifth of the ordering cost)

The boost converter module is used in the energy input circuit to increase the charge voltage of the charge storage module, allowing for higher overall energy storage. From the specifications provided by the product page for the selected boost converter module shown in Fig. 4 above and from our tests of the module we received, the module is capable of delivering an output voltage of approximately 16V to the current limiter circuit at currents of at least 3.2A, as shown in the test conducted in Fig. 5 below. The boost converter module did increase the overall current draw above the approximately 3A used to charge the energy storage module, but as is shown below, the total current draw did not exceed the wired charger limit of 5A. When used for wireless charging however, the overall system did experience inrush current issues which were not accounted for in the initial design and were not able to be fixed by the time of the competition, as is discussed later in the Reflections and Conclusions section.



Figure 5: Boost converter module measurements at 16V output, 12V input, and an output current of 3.2A, demonstrating an input current draw below the rated 5A limit of the provided 12V chargers



Figure 6: Current limiter circuit schematic showing mode-toggling relay



Figure 7: Pspice Schematic for 3A current limiter



Figure 8: PSpice simulation results for 3A current limiter, created by sweeping load current I1 and observing the voltage shutoff that occurs at approximately 3.2A, which fits our design requirements



Figure 9: PSpice schematic for 1.5A current limiter (All parts of the schematic are kept the same except for the short across R6 to simulate the behavior of the mode-switching relay when the wired charger is unplugged)



Figure 10: PSpice simulation results for 1.5A current limiter, created by sweeping load current I1 and observing the voltage shutoff that occurs at approximately 1.4A, which fits our design requirements

#### **Charge balance and energy storage**



Figure 11: Energy storage and balancing circuit schematic

The energy storage and balancing circuit can be mapped to the store energy and balance energy blocks of the functional architecture. The energy storage design allows for six 100F capacitors to be charged in series to supply a voltage of 15V as found in Figure 11. In order to meet safety requirements S1, the charge balancing circuit prevents leakage current from damaging the supercapacitors, a charge balancing circuit is necessary. The charge balancing design uses a 1N4678 zener diode and darlington pair combination of a TIP41B which is rated for 6A and a 2N4403 transistor. The supercapacitors to be used are portrayed in Figure 12. This design was chosen as opposed to a singular zener diode, as the available diodes on the market rated for a high enough current provided by the current limiting circuit were too expensive. When the zener diode reaches 1.8V, it shunts the capacitor and prevents it from overcharging.



Figure 12: Supercapacitor used in the power supply schematics

**Balancing circuit**



Figure 13: charge balancing circuit stage

The individual charge balancing circuit for a single supercapacitor can be found in Figure 13. The PSpice schematic for the wired and wireless chargers can be found below in Figure 14 and Figure 16. The wired charger is shown to charge within 2.5 minutes, and the wireless charger similarly charges within 6 minutes as found in Figure 16 and Figure 18.



Figure 14: Pspice circuit model for capacitor charging using the wired charger



Figure 15: Simulation of wired-current charging of the energy storage system demonstrating that no capacitor reaches a potential difference greater than their rated 2.7V maximum



Figure 16: Pspice circuit model for capacitor charging using the wireless charger



Figure 17: Simulation of wireless-current charging of the energy storage system demonstrating that no capacitor reaches a potential difference greater than their rated 2.7V maximum

#### **Energy Output System**



DZS Elec DC 4A Constant Voltage and Current Step-Up Down Power Supply Module Adjustable Automatic DC-DC 5V-30V to 0.5V-30V Regulated Power Supply Charging Converter Buck/Boost Voltage Regulator

Figure 18: Energy output buck-boost module

The energy output circuit can be mapped to the control discharging block of the functional architecture. By using a buck-boost converter rated for our expected input voltages of 5V-15V at least 2A, it is possible to regulate the voltage provided to the controller. From the specifications provided by the product page for our selected buck-boost converter module shown in Fig. 18 above and from our tests of the module we received, the module is capable of meeting these input voltage and current expectations while delivering a steady 7.6V supply to the motor controller at currents greater than 2A. When the capacitors discharge below approximately 5V, the buck-boost converter cuts off, deactivating the output current and dropping the output voltage to 0V, but by this point the car should have completed the race, therefore meeting the 90s requirement.



Figure 19: Buck-Boost converter module measurements at 15V input, 7.6V output, and an output current of 2A

## **Value Feature**







Figure 21: LED Headlight implementation on the vehicle

The additional value feature added to the system is a headlight feature as depicted in Fig. 21 and Fig. 22 which has been placed at the front of the car to improve the visibility of the line, which will in turn increase the reliability of our line following algorithm, thereby satisfying requirement V1.0.

# **Safety Feature**



Figure 22: Final implementation of the power supply safety shield

The additional safety feature for the system is a safety shield designed to prohibit unintentional access to the terminals of the supercapacitors or to any other dangerous exposed terminals present on the final physical design implementation. This system completes our previously defined safety requirement as defined in requirement S4, and was provided to us for free thanks to Gary Meyer and Mark Crosby.





Figure 23: Plot of final power supply charging from the wired charger



Figure 24: Plot of final power supply discharging at a constant 1.2A current draw

Assembling all of the components discussed above, we were able to produce a supercapacitor power supply that was capable of charging up to its maximum voltage well within the required time and discharging to provide more than the current required by the vehicle for well above the time requirements of the competition, as shown in Fig. 23 and Fig. 24 above.

# **Appendix**

## **Bill of materials**









# **Reflections and Conclusions**







We were capable of constructing a functional wired power supply, however looking back on the project, there were a few obstacles in our design process that prevented us from meeting a few specifications. Our initial design for the current limiter used inverted comparator logic, causing the op amp we had used to burn out from needing to constantly supply large amounts of current in order to keep the Darlington pair conductive. To fix this issue, we remade the current limiter circuit as an independent module using perfboard and parts from the parts room and then mounted it on top of the section of our old PCB where the original current limiter circuit was. While our design was modular, we did not optimize the means by which we dealt with heat dissipation and in doing so used more heat sinks than necessary. This significantly increased the weight of the car which prevented it from driving up the hill on the oval track. Furthermore, during the day of the competition, there were mechanical issues with our car's power-delivery belt that worsened the car's ability to climb inclined surfaces. Additionally, the chassis of our car was broken for a majority of this design project – we had implemented our own suspension system. When we went to get our belt tightened, the suspension we had been using was also fixed and without adequate time in between the fix and the competition to optimize the controller with the final power supply combined with the difference in Kahn room lighting meant that our vehicle suffered from instability issues during the final competition that had not been taken into account during the initial design of the controller in the laboratory in the NAB. Had we had enough time to tune our controller to accommodate for the changing environmental factors we would have likely seen better results regardless of our headlight value feature that was meant to eliminate that variable.